### Revision Lecture 2: Transients & Lines

- Transients: Basic Ideas
- Steady States
- Determining Time

#### Constant

- Determining Transient
- Amplitude
- Transmission Lines Basics
- Reflections
- Sinewaves and Phasors
- Standing Waves

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  - Input voltage/current abruptly changes its magnitude, frequency or phase
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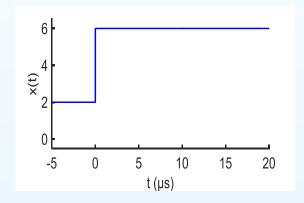
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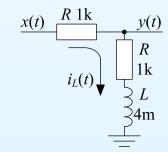
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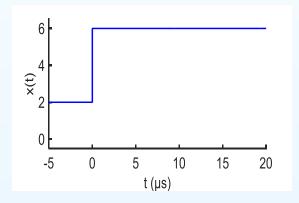


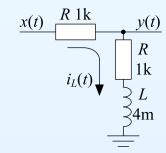


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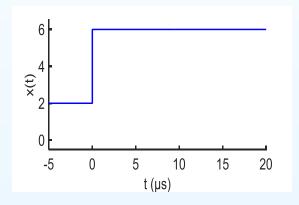
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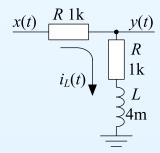
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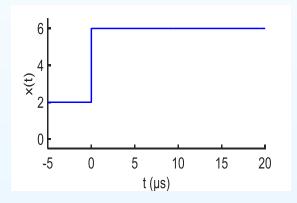
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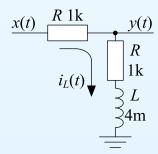
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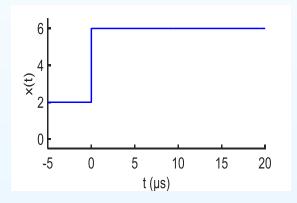
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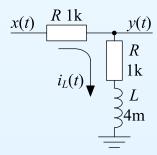
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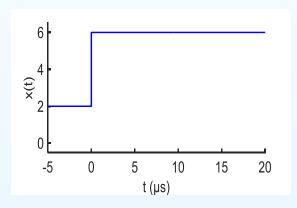
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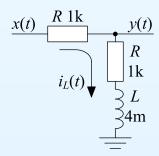
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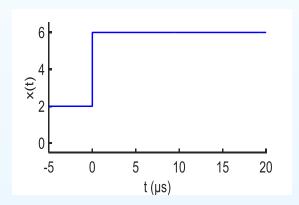
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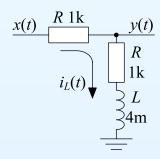
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 set  $\omega = 0$ :  $\frac{Y}{X}(0) = \frac{1}{2}$ 





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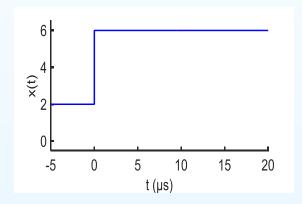
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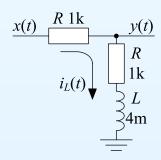
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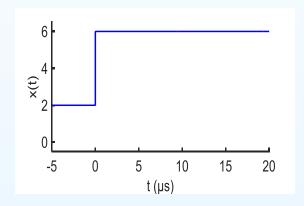
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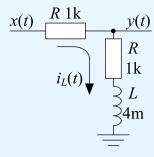
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$$\begin{split} \frac{Y}{X}(j\omega) &= \frac{R+j\omega L}{2R+j\omega L}\\ \text{set } \omega &= 0 \colon \frac{Y}{X}(0) = \frac{1}{2}\\ y_{SS}(0-) &= 1, y_{SS}(0+) = 3 \end{split}$$



Sinusoidal input  $\Rightarrow$  Sinusoidal steady state  $\Rightarrow$  use phasors.

Then convert phasors to time waveforms to calculate the actual output voltages  $y_{SS}(0-)$  and  $y_{SS}(0+)$  at t=0.

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Method 1: Thévenin x(t) = 4R x(t) = 4R

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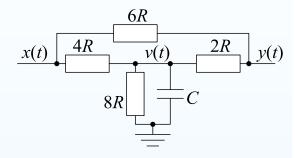
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Method 1: Thévenin

(a) Remove the capacitor/inductor



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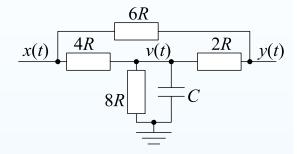
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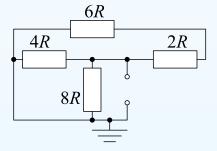
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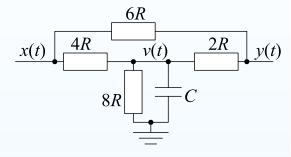
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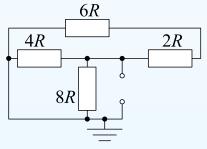
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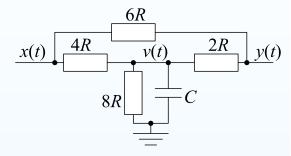
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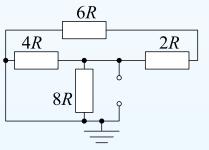
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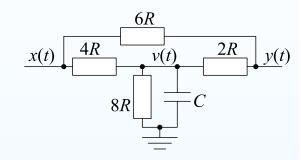
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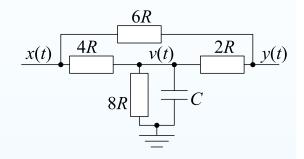
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KCL @ V: 
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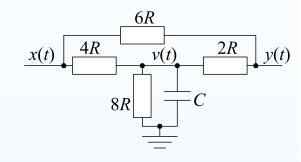
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ightarrow Eliminate V to get transfer Function:  $\frac{Y}{X} = \frac{8j\omega RC + 13}{32j\omega RC + 16}$ 

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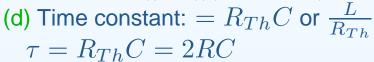
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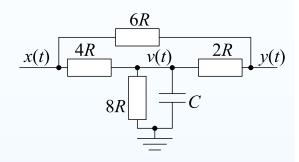
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$$\frac{Y-V}{2R}+\frac{Y-X}{6R}=0$$

- ightarrow Eliminate V to get transfer Function:  $\frac{Y}{X} = \frac{8j\omega RC + 13}{32j\omega RC + 16}$
- (b) Time Constant =  $\frac{1}{\text{Denominator corner frequency}}$

### Revision Lecture 2: Transients & Lines

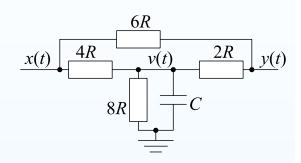
- Transients: Basic Ideas
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#### Method 1: Thévenin

- (a) Remove the capacitor/inductor
- (b) Set all sources to zero (including the input voltage source). Leave output unconnected.
- (c) Calculate the Thévenin resistance between the capacitor/inductor terminals:

$$R_{Th}=8R||4R||(6R+2R)=2R$$
 (d) Time constant:  $=R_{Th}C$  or  $\frac{L}{R_{Th}}$ 

$$\tau = R_{Th}C = 2RC$$



#### Method 2: Transfer function

(a) Calculate transfer function using nodal analysis

KCL @ V: 
$$\frac{V-X}{4R} + \frac{V}{8R} + j\omega CV + \frac{V-Y}{2R} = 0$$
 KCL @ Y:  $\frac{Y-V}{2R} + \frac{Y-X}{6R} = 0$ 

$$ightarrow$$
 Eliminate  $V$  to get transfer Function:  $\frac{Y}{X} = \frac{8j\omega RC + 13}{32j\omega RC + 16}$ 

(b) Time Constant =  $\frac{1}{\text{Denominator corner frequency}}$ 

$$\omega_d = \frac{16}{32RC} \Rightarrow \tau = \frac{1}{\omega_d} = 2RC$$

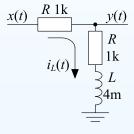
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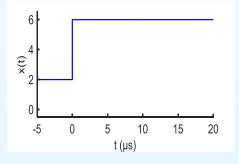
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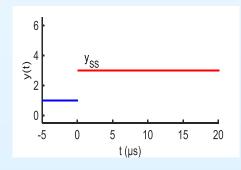
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After an input change at t=0,  $y(t)=y_{SS}(t)+Ae^{-\frac{t}{\tau}}$ .







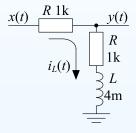
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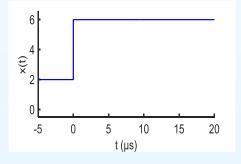
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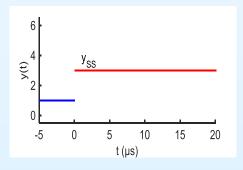
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After an input change at t = 0,  $y(t) = y_{SS}(t) + Ae^{-\frac{t}{\tau}}$ .  $\Rightarrow y(0+) = y_{SS}(0+) + A \Rightarrow A = y(0+) - y_{SS}(0+)$ 







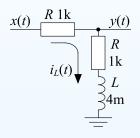
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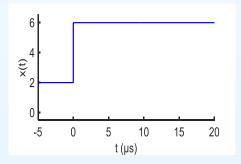
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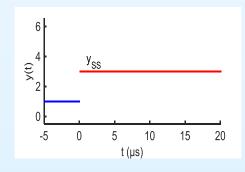
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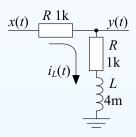
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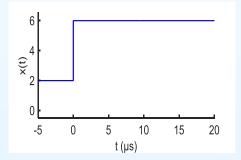
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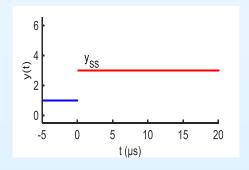
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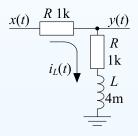
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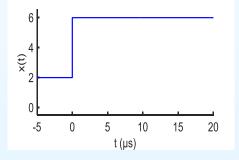
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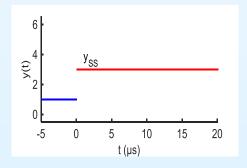
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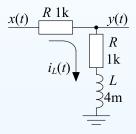
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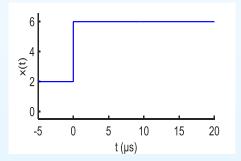
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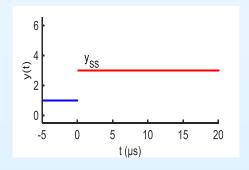
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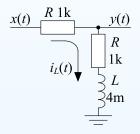
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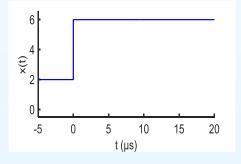
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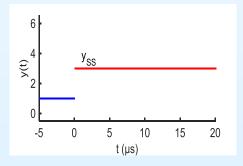
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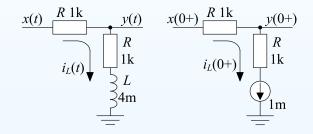
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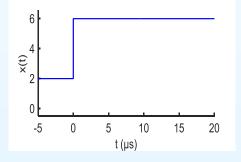
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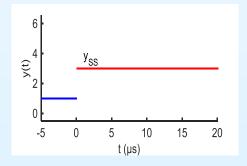
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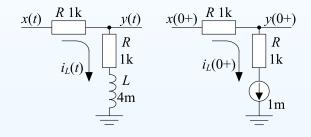
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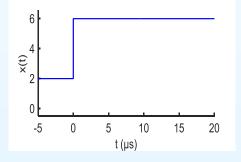
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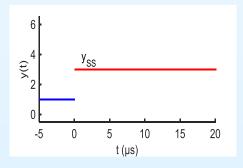
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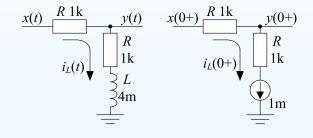
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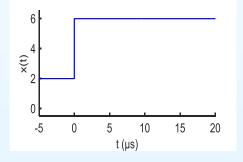
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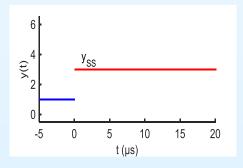
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- (i) Version 2: Transfer function







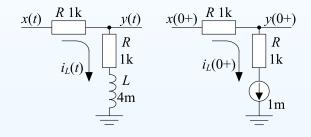
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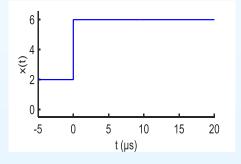
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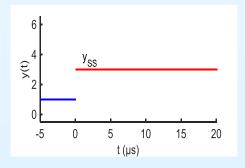
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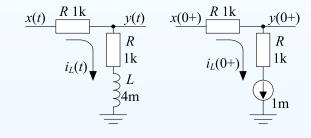
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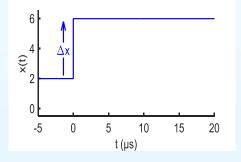
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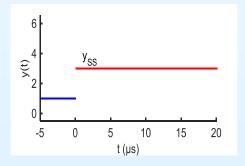
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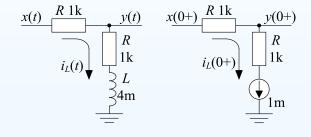
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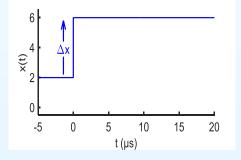
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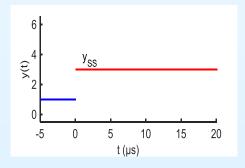
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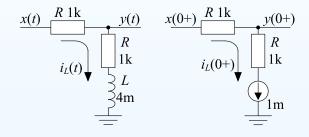
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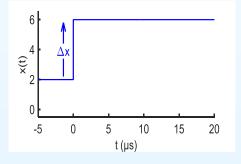
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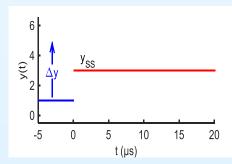
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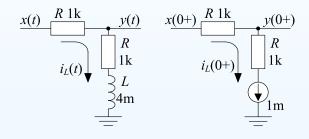


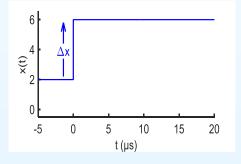
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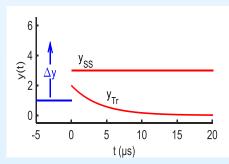
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- (ii)  $A = y(0+) y_{SS}(0+) = 5 3 = 2$





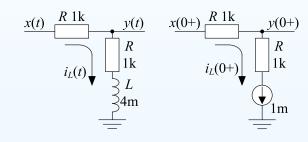


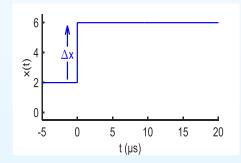
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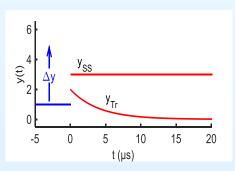
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- (iii)  $y(t) = y_{SS}(t) + Ae^{-t/\tau}$







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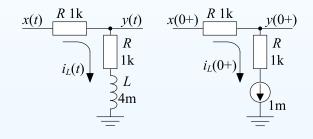
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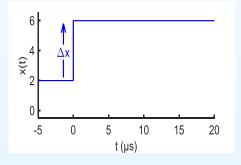
After an input change at t=0,  $y(t)=y_{SS}(t)+Ae^{-\frac{t}{\tau}}$ .  $\Rightarrow y(0+)=y_{SS}(0+)+A\Rightarrow A=y(0+)-y_{SS}(0+)$  Method: (a) calculate true output y(0+), (b) subtract  $y_{SS}(0+)$  to get A

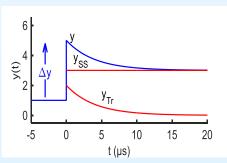
- (i) Version 1:  $v_C$  or  $i_L$  continuity  $x(0-)=2\Rightarrow i_L(0-)=1~\mathrm{mA}$  Continuity  $\Rightarrow i_L(0+)=i_L(0-)$  Replace L with a  $1~\mathrm{mA}$  current source y(0+)=x(0+)-iR=6-1=5
- (i) Version 2: Transfer function  $H(j\omega) = \frac{Y}{X}(j\omega) = \frac{R+j\omega L}{2R+j\omega L}$  Input step,  $\Delta x = x(0+) x(0-) = +4$   $y(0+) = y(0-) + H(j\infty) \times \Delta x$   $= 1 + \Delta y = 1 + 1 \times 4 = 5$

(ii) 
$$A = y(0+) - y_{SS}(0+) = 5 - 3 = 2$$

(iii)  $y(t) = y_{SS}(t) + Ae^{-t/\tau}$ =  $3 + 2e^{-t/2\mu}$ 







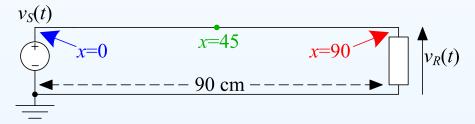
Revision Lecture 2: Transients & Lines

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Transmission Line: constant  ${\cal L}_0$  and  ${\cal C}_0$ : inductance/capacitance per metre.

Forward wave travels along the line:  $f_x(t) = f_0\left(t - \frac{x}{u}\right)$ .

Velocity 
$$u = \sqrt{\frac{1}{L_0 C_0}} \approx \frac{1}{2}c = 15 \, \mathrm{cm/ns}$$



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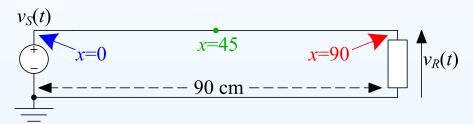
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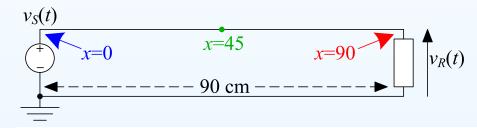
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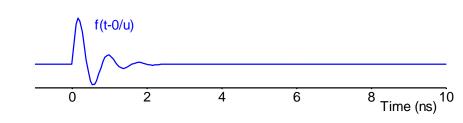
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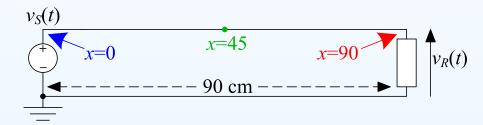
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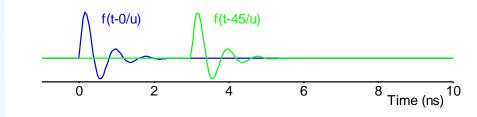
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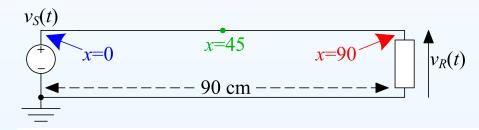
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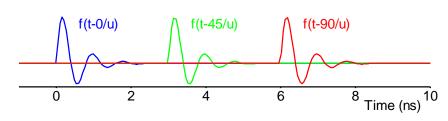
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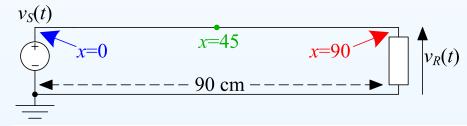
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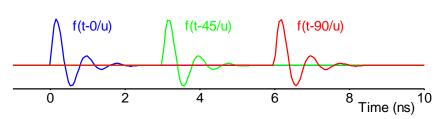
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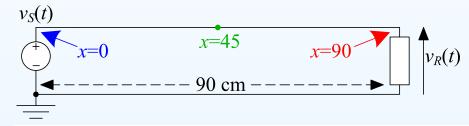
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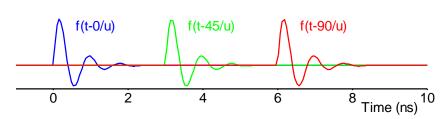
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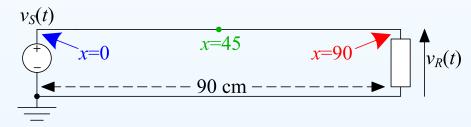
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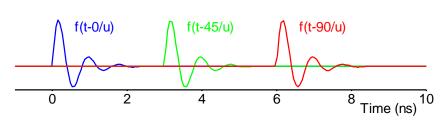
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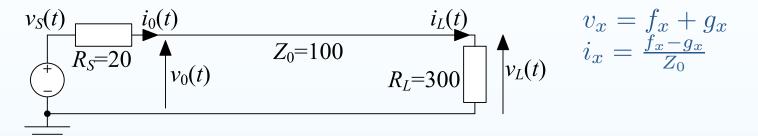
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Waveforms of  $f_x$  and  $g_x$  are determined by the connections at both ends.

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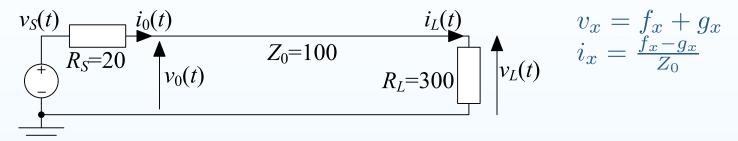
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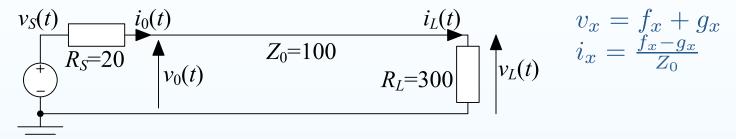


At 
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, Ohm's law  $\Rightarrow \frac{v_L(t)}{i_L(t)}=R_L \ \Rightarrow g_L\left(t\right)=\frac{R_L-Z_0}{R_L+Z_0} \times f_L\left(t\right)$ .

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$$v_S(t)$$
 $R_S=20$ 
 $v_0(t)$ 
 $v_0(t)$ 
 $v_L(t)$ 
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$$v_{S}(t) = i_{0}(t)$$

$$R_{S}=20$$

$$v_{0}(t)$$

$$V_{L}(t)$$

$$v_{x} = f_{x} + g_{x}$$

$$i_{x} = \frac{f_{x} - g_{x}}{Z_{0}}$$

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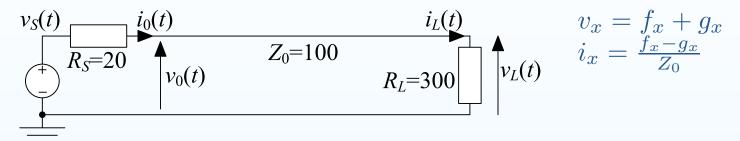
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At 
$$x = 0$$
:  $f_0(t) = \frac{Z_0}{R_S + Z_0} v_S(t) + \frac{R_S - Z_0}{R_S + Z_0} g_0(t)$ 

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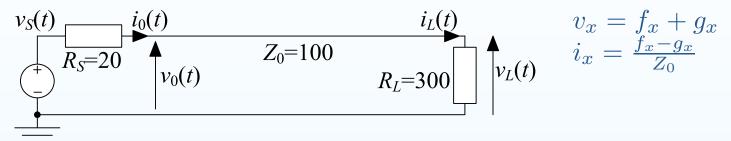
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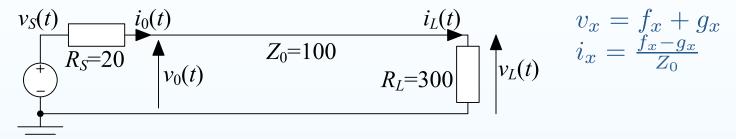
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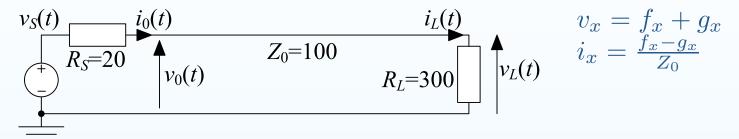
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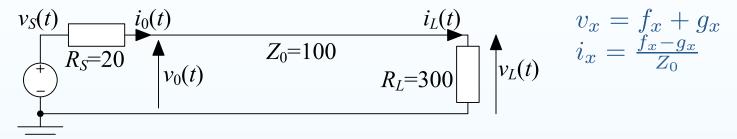
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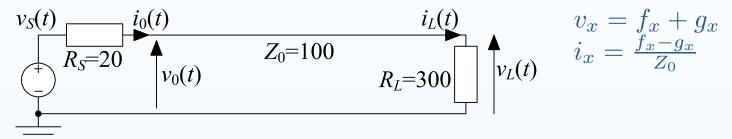
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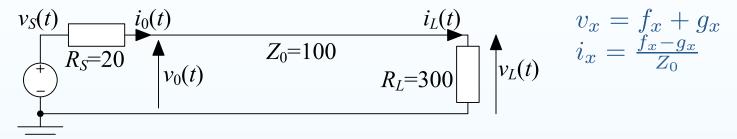
$$v_S(t) \xrightarrow{\times \tau_0} f_0(t) \xrightarrow{\times \rho_L} g_0(t + \frac{2L}{u}) \xrightarrow{\times \rho_0} f_0(t + \frac{2L}{u}) \xrightarrow{\times \rho_L} g_0(t + \frac{4L}{u})$$

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- Transients: Basic Ideas
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- Standing Waves



At 
$$x=L$$
, Ohm's law  $\Rightarrow \frac{v_L(t)}{i_L(t)}=R_L \Rightarrow g_L(t)=\frac{R_L-Z_0}{R_L+Z_0}\times f_L(t)$ .

Reflection coefficient:  $\rho_L = \frac{g_L(t)}{f_L(t)} = \frac{R_L - Z_0}{R_L + Z_0}$   $\rho_L \in [-1, +1]$  and increases with  $R_L$ 

Knowing  $f_x(t)$  for  $x=x_0$  now tells you  $f_x,\ g_x,\ v_x,\ i_x\ \forall x$ 

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$$x=0$$
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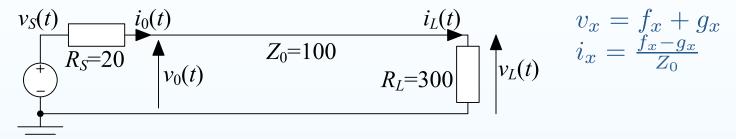
$$v_S(t) \xrightarrow{\times \tau_0} f_0(t) \xrightarrow{\times \rho_L} g_0(t + \frac{2L}{u}) \xrightarrow{\times \rho_0} f_0(t + \frac{2L}{u}) \xrightarrow{\times \rho_L} g_0(t + \frac{4L}{u}) \xrightarrow{\times \rho_0} \cdots$$

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Wave bounces back and forth getting smaller with each reflection:

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Infinite sum:

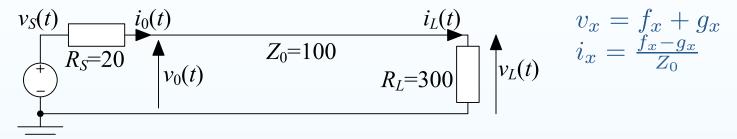
$$f_0(t) = \tau_0 v_S(t) + \tau_0 \rho_L \rho_0 v_S(t - \frac{2L}{u}) + \dots$$

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Infinite sum:

$$f_0(t) = \tau_0 v_S(t) + \tau_0 \rho_L \rho_0 v_S(t - \frac{2L}{u}) + \ldots = \sum_{i=0}^{\infty} \tau_0 \rho_L^i \rho_0^i v_S(t - \frac{2Li}{u})$$

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Sinewayes are easier because:

- 1. Use phasors to eliminate t:
- 2. Time delays are just phase shifts:

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As before: 
$$V_x = F_x + G_x$$
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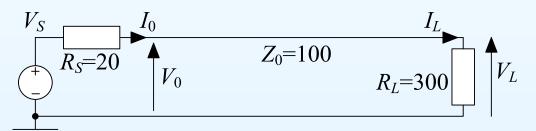
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$$\begin{bmatrix} \bullet \\ V_L \end{bmatrix} V_L \qquad G_L = \rho_L F_L \\ F_0 = \tau_0 V_S + \rho_0 G_0$$

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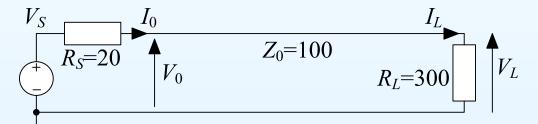
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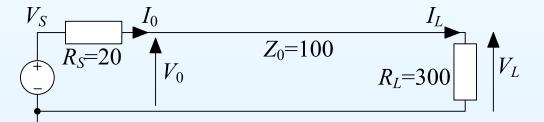
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As before:

 $V_L \qquad G_L = \rho_L F_L$  $F_0 = \tau_0 V_S + \rho_0 G_0$ 

But  $G_0=F_0\rho_Le^{-2jkL}$ : roundtrip delay of  $\frac{2L}{u}$  + reflection at x=L. Substituting for  $G_0$  in source end equation:  $F_0=\tau_0V_S+\rho_0F_0\rho_Le^{-2jkL}$ 

#### **Revision Lecture 2:** Transients & Lines

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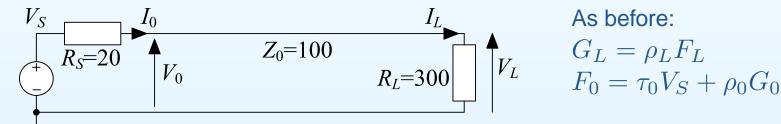
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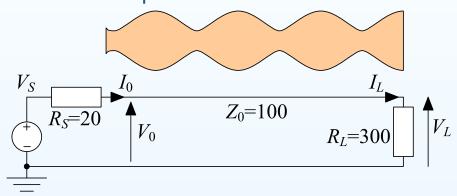
$$G_L = \rho_L F_L$$
  
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Standing waves arise whenever a wave meets its reflection: at positions where the two waves are in phase their amplitudes add but where they are anti-phase their amplitudes subtract.

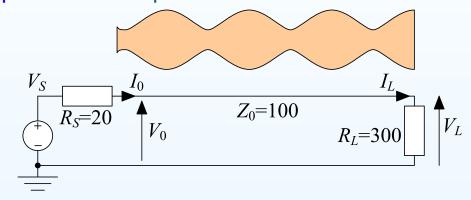


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At any point x, delay of  $\frac{x}{u} \Rightarrow$   $F_x = F_0 e^{-jkx}$ 

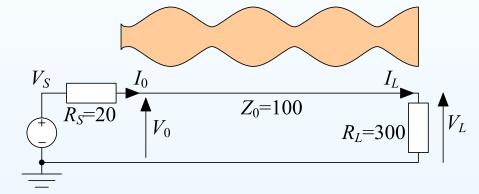


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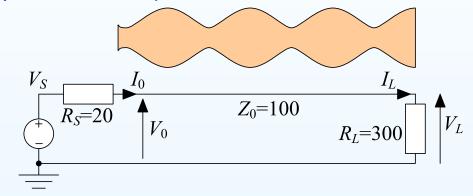
Backward wave:  $G_x = \rho_L F_x e^{-2jk(L-x)}$ 

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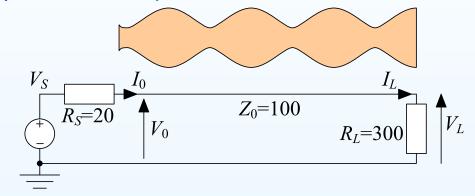
Backward wave:  $G_x = \rho_L F_x e^{-2jk(L-x)}$ : reflection + delay of  $2\frac{L-x}{u}$ 

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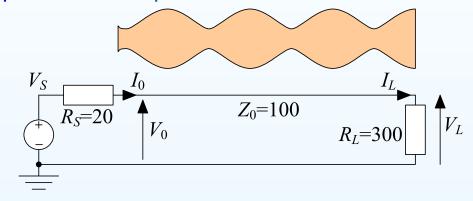
Voltage at x:  $V_x = F_x + G_x$ 

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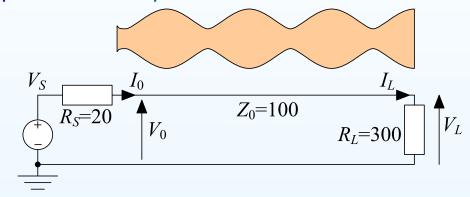
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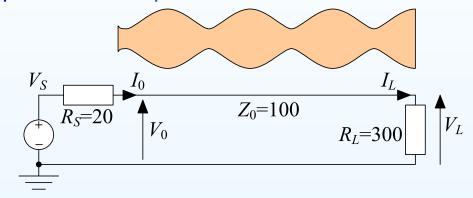
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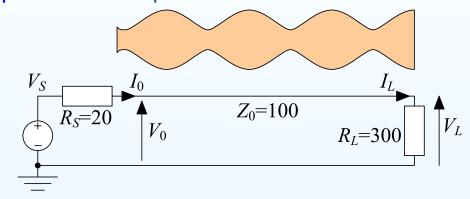
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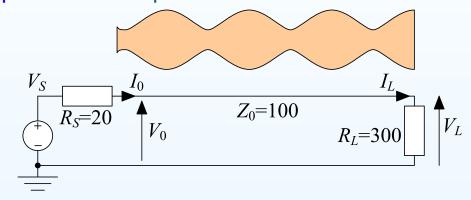
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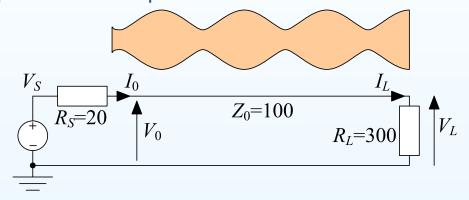
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At any point x, delay of  $\frac{x}{u} \Rightarrow$   $F_x = F_0 e^{-jkx}$ 



Backward wave:  $G_x = \rho_L F_x e^{-2jk(L-x)}$ : reflection + delay of  $2\frac{L-x}{u}$  Voltage at x:  $V_x = F_x + G_x = F_0 e^{-jkx} \left(1 + \rho_L e^{-2jk(L-x)}\right)$  Voltage Magnitude :  $|V_x| = |F_0| \left|1 + \rho_L e^{-2jk(L-x)}\right|$ : depends on x

If  $\rho_L \geq 0$ , max magnitude is  $(1+\rho_L) |F_0|$  whenever  $e^{-2jk(L-x)} = +1$   $\Rightarrow x = L$  or  $x = L - \frac{\pi}{k}$  or  $x = L - \frac{2\pi}{k}$  or . . .

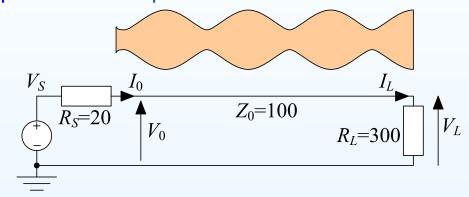
Min magnitude is  $(1 - \rho_L) |F_0|$  whenever  $e^{-2jk(L-x)} = -1$ 

Revision Lecture 2: Transients & Lines

- Transients: Basic Ideas
- Steady States
- Determining Time
   Constant
- Determining Transient Amplitude
- Transmission Lines Basics
- Reflections
- Sinewaves and Phasors
- Standing Waves

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